## Chapter 7

7.1 (a) Prove that Howe's result, equation 7.3.4, is consistent with the Kutta-Joukowski theorem, equation 2.7.23, by considering first a line vortex of strength $\Gamma$, parallel to $x_{3}$, located at $x_{2}=h$, and traveling in the $x_{1}$ direction at speed $U$
(b) Consider a two-dimensional circular cylinder centered on the $x_{3}$ axis of radius $R$. Determine the unsteady force components per unit span exerted by the cylinder on the fluid, as functions of time, due to the passage of the above line vortex in the $x_{1}$ direction at speed $U$. Assume there is no circulation generated around the cylinder.
(c) Plot the time trace of the force components, normalized on $\rho_{o} U \Gamma$ as a function of normalized time $t U / R$ from -2 to 2 , for $h / R=1.5$.
(d) What equation would you use to determine the far field sound radiated by a small acoustically compact spanwise portion of the cylinder?

Worked example solution

## Solution Problem 7.1

(a) Equation 7.3.4 gives the force applied to the fluid by a body as

$$
F_{i}=-\rho_{o} \int_{V} \nabla Y_{i} .(\boldsymbol{\omega} \times \mathbf{v}) d V
$$

Consider a line vortex of strength $\Gamma$ parallel to the $x_{3}$ axis located at $x_{2}=h$ and traveling along the $x_{1}$ axis at speed $U$. For this we have

$$
\boldsymbol{\omega}=\Gamma \delta\left(x_{1}-U t\right) \delta\left(x_{2}-h\right) \mathbf{e}_{3}
$$

where $\mathbf{e}_{\mathbf{i}}$ denotes the unit vector in the direction of $x_{i}$. The velocity of the vortex $\mathbf{v}=U \mathbf{e}_{\mathbf{1}}$, and so

$$
(\boldsymbol{\omega} \times \mathbf{v})=U \Gamma \delta\left(x_{1}-U t\right) \delta\left(x_{2}-h\right) \mathbf{e}_{2}
$$

Clearly, therefore, the vortex can only generate a force in the $x_{2}$ direction. Consider thus the Kirchhoff coordinate for a unit free stream in the $x_{2}$ direction, which will give $\nabla Y_{2}=\mathbf{e}_{2}$, and so

$$
F_{2}=-\rho_{o} \int_{V} U \Gamma \delta\left(x_{1}-U t\right) \delta\left(x_{2}-h\right) d V
$$

and so the force per unit span in the $x_{3}$ direction is

$$
f_{2}=-\rho_{o} U \Gamma
$$

Now, if we change our frame of reference to be traveling with the vortex then we will see a free stream in the $x_{1}$ direction of velocity $U_{\infty}=-U$. Therefore, in terms of this free stream velocity, we have

$$
f_{2}=\rho_{o} U_{\infty} \Gamma
$$

This recall is the force on the fluid. Thus the force on the vortex must be,

$$
f_{2}=-\rho_{o} U_{\infty} \Gamma
$$

(b) For this problem we need to determine the Kirchhoff coordinate gradient $\nabla Y_{i}$ for the flow in the $x_{i}$ direction around the cylinder. To get both $F_{1}$ and $F_{2}$ components we will have to consider $i=1,2$. The complex velocity for acyclic flow past a circular cylinder is given by equation 2.7.16,

$$
w^{\prime}(z)=e^{-i \alpha}-\frac{R^{2} e^{i \alpha}}{z^{2}}
$$

Where we have taken $U_{\infty}=1$ and where $\alpha=0$ for $i=1$ and $\alpha=\pi / 2$ for $i=2$. Now,

$$
\nabla Y_{i}=\operatorname{Re}\left\{w^{\prime}(z)\right\} \mathbf{e}_{\mathbf{1}}-\operatorname{Im}\left\{w^{\prime}(z)\right\} \mathbf{e}_{\mathbf{2}}
$$

So,

$$
\nabla Y_{i} \cdot(\boldsymbol{\omega} \times \mathbf{v})=-\operatorname{Im}\left\{w^{\prime}(z)\right\} U \Gamma \delta\left(x_{1}-U t\right) \delta\left(x_{2}-h\right)
$$

Now,

$$
\begin{aligned}
\operatorname{Im}\left\{w^{\prime}(z)\right\} & =-\sin \alpha-\operatorname{Im}\left\{\frac{R^{2}(\cos \alpha+i \sin \alpha)\left(x_{1}^{2}-x_{2}^{2}-2 i x_{1} x_{2}\right)}{r^{4}}\right\} \\
& =-\sin \alpha-\frac{R^{2}}{r^{4}}\left[\left(x_{1}^{2}-x_{2}^{2}\right) \sin \alpha-2 x_{1} x_{2} \cos \alpha\right]
\end{aligned}
$$

where $r^{2}=x_{1}^{2}+x_{2}^{2}$. So,

$$
f_{i}=-\rho_{o} U \Gamma\left\{\sin \alpha+\frac{R^{2}}{\left(U^{2} t^{2}+h^{2}\right)^{2}}\left[\left(U^{2} t^{2}-h^{2}\right) \sin \alpha-2 U t h \cos \alpha\right]\right\}
$$

So,

$$
f_{1}=\rho_{o} U \Gamma \frac{2 U t h R^{2}}{\left(U^{2} t^{2}+h^{2}\right)^{2}}
$$

and

$$
f_{2}=-\rho_{o} U \Gamma\left\{1+\frac{R^{2}\left(U^{2} t^{2}-h^{2}\right)}{\left(U^{2} t^{2}+h^{2}\right)^{2}}\right\}
$$

(c) The above expressions are normalized as

$$
\frac{f_{1}}{\rho_{o} U \Gamma}=\frac{2 \frac{U t}{R} \frac{h}{R}}{\left(\left[\frac{U t}{R}\right]^{2}+\left[\frac{h}{R}\right]^{2}\right)^{2}}
$$

and

$$
\frac{f_{2}}{\rho_{o} U \Gamma}=-1-\frac{\left(\left[\frac{U t}{R}\right]^{2}-\left[\frac{h}{R}\right]^{2}\right)}{\left(\left[\frac{U t}{R}\right]^{2}+\left[\frac{h}{R}\right]^{2}\right)^{2}}
$$

Plotting code and plot:

```
clear all; close all;
tn=-2:.01:2;
hR=1.5;
f1n=2*tn*hR./(tn.^2+hR.^2).^2;
f2n=-1-(tn.^2-hR.^2)./(tn.^^2+hR.^2).^2;
figure
subplot(2,1,1)
plot(tn,f1n,'k-');
xlabel('tU/R');ylabel('f_1/\rho_oU\Gamma');
subplot(2,1,2)
plot(tn,f2n,'k-');
xlabel('tU/R');ylabel('f_2/\rho_oU\Gamma');
```



(d) Equation 4.4.7

$$
p^{\prime}=\frac{x_{i}}{4 \pi|\mathbf{x}|^{2} c_{\infty}} \frac{\partial F_{i}}{\partial t}
$$

